

# catool

Combustion Analysis TOOL

User Guide

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catool ([www.catool.org](http://www.catool.org))

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## **Introduction**

Catool is an open-source software package designed to post-process cylinder pressure data collected from an internal combustion engine. As well as calculating standard thermodynamic calculations such as pressure rise rates, heat transfer and knock metrics, it deals with the format conversion, absolute pressure referencing, error detection and correction required for robust data analysis.

Catool can import raw combustion data from the industry standard AVL I-File format as well as ASCII text files, allowing the flexibility to use off-the-shelf data acquisition systems such as those from National Instruments and Measurement Computing, to standard combustion systems such as AVL Indiscope and ADAPT CAS.

Catool has been designed to be fast, flexible and capable of simple modification to suit a range of combustion analysis tasks. Its primary limitation is that of available memory, it does not have built-in limitations on the number of channels or lengths of data acquisition.

## Downloading and Installation

The latest version of catool can be downloaded from [www.catool.org](http://www.catool.org). It is available both as source code for compilation on Unix type operating systems or pre-compiled binaries for Microsoft Windows.

By providing source code, catool can be compiled to run on almost any operating system and can easily be modified to suit particular purposes.

By providing pre-compiled binaries for Microsoft Windows, most users can be up and running in a matter of minutes.

### Source code and Compiling

If you wish to install catool out-of-the-box on a Microsoft Windows platform you can skip to the Binary Installation section.

### Compiling in a UNIX environment

Replace the # with the latest version number of catool:

```
mkdir /usr/src/catool-2.0
cd /usr/src/catool-2.0
wget https://catool.org/files/catool-2.0-src.zip
unzip catool-2.0-src.zip
make clean
make
```

catool should now be built. Check by running

```
./catool
```

You should see the following output

```
Usage: catool [-h] [--debug-level=<debug_level>] file
```

### Binary Installation

Once you have compiled or downloaded the catool binary this needs to be copied to a suitable working directory. On a UNIX platform this could be perhaps `/usr/bin`, on a Windows platform `C:\catool`. In a Windows environment you need to copy both the `catool.exe` and `vcruntime.dll` files to your computer.

# Background

## Crank Angle Domain

Unlike most traditional data analysis, combustion analysis is performed in the crank angle domain.

Data can be stored using up to five variable resolutions through an engine cycle. This minimises storage and processing, so for example, data can be stored at 1 degree resolution for the intake and compression strokes, 0.2 degree resolution for the first 40 degrees of the expansion stroke and the remaining at 1 degree resolution. A high resolution in this case enables robust knock detection.

Catool uses the following nomenclature regarding crank angles:

*degrees* – number of degrees from intake TDC, therefore:

Intake stroke - -360 to -180 degrees

Compression stroke – -180 to 0 degrees

Expansion stroke – 0 to 180 degrees

Exhaust stroke – 180 to 360 degrees

*Note that in versions prior to 0.9.8 the nomenclature of degrees ranged from 0 to 720 for a four stroke cycle. This has been changed in line with general industry practice of -360 to +360 degrees. Existing configuration files will need their angular references modified by subtracting 360 degrees for a four stroke engine or 180 degrees for a two stroke engine.*

*theta* – these are units of the lowest resolution supported by catool. As standard this is set as 1/20<sup>th</sup> of a degree. For a four stroke engine cycle theta therefore ranges from 0 to 14400 ( 720 degrees \* 20 theta/degree).

*crank\_angle* – data referenced in the crank\_angle domain is in sequential order. This is important to understand when the crank\_angle abscissa has multiple measurement tables. For simple 1 degree resolution data crank\_angle would range from 0 to 720. For data with a multiple resolution abscissa, for example 0 to 360 degrees @ 1 degree resolution, 360 to 400 degrees @ 0.2 degree resolution and 400 to 720 degrees @ 1 degree resolution there would be 880 crank\_angle data points.

## **Cycles**

Crank angle data is stored for a number of engine cycles. One cycle being two revolutions for a four stroke engine.

Catool's analysis is stored either in the crank angle domain, such as mean gas temperature and on a cyclic based, such as peak mean gas temperature. Catool also calculates statistics based over the entire set of engine cycles.

## **Configuration file**

Catool is a command line driven program using a configuration file to configure the file input/output and analysis to be run. The configuration file is in text format and can be edited using Notepad or WordPad in Windows.

## Usage

Catool is invoked from the command line.. This is either the Windows or UNIX command prompt

### Windows

Open the command prompt by opening Start, All Programs, Accessories, Command Prompt.

Microsoft Windows XP [Version 5.1.2600]  
(C) Copyright 1985-2001 Microsoft Corp.

```
C:\>cd catool
```

```
C:\catool>catool rover_v8_csv.ccf
```

Combustion Analysis Tool (catool)  
Copyright (C) Ben Brown, 2000-2009  
Version 0.9.7  
www.catool.org

catool incorporates code from Pthreads-win32 ([sourceware.org/pthreads-win32](http://sourceware.org/pthreads-win32))  
Copyright (C) 1998 John E. Bossom  
Copyright (C) 1999,2006 Pthreads-win32 contributors

Config File: rover\_v8\_csv.ccf  
Debug level: NOTICE  
Set input filetype to CSV  
Set input abscissa type to CRANK\_ANGLE  
[cut]

Analysis complete

```
C:\catool>
```

## Examples

The following examples use some combustion data recorded from a Rover V8 engine. The raw data is available at <https://catool.org/files/roverv8-2000rpm-wot.zip>

### **Rover V8 CSV – Load, Analyse, Save**

Download the example configuration from [https://catool.org/files/rover\\_v8\\_csv.ccf](https://catool.org/files/rover_v8_csv.ccf)

### **Rover V8 AVL – Load, Analyse, Save**

Download the example configuration from [https://catool.org/files/rover\\_v8\\_avl.ccf](https://catool.org/files/rover_v8_avl.ccf). This uses the AVL I-File generated in the above CSV example.

### **Rover V8 AVL – Load, Save as MATLAB**

Download the example configuration from [https://catool.org/files/avl\\_matlab.ccf](https://catool.org/files/avl_matlab.ccf).

### **Loading IFile data directly into MATLAB**

See here <https://catool.org/documentation.html>.



## Reference

The following are valid parameters in the catool configuration file:

```
debug-level ( DEBUG | NOTICE | WARNING | ERROR | FATAL | SILENT )
```

This configures the amount of output catool displays on the screen ranging from very comprehensive (DEBUG) to nothing (SILENT). This parameter can also be specified at the command line:

```
catool -debug-level=WARNING config.ccf
```

In specifying the debug level as a command line option, any use in the config file will have no effect.

```
input-file-type ( IFILE | CSV )
```

This specifies the type of file catool will be loading next.

```
input-file <filename>
```

This specifies the file which will be used to load data. You should specify the type of file with `input-file-type` before this command as catool will load the file header and initialise various data structures ready to load any channels.

```
error-check ( on | off )
```

Turn error checking on or off. Default is off. If a result falls outside of a range specified in the `cat.h` file then a warning message will be displayed.

```
input-abscissa-type ( CRANK_ANGLE | CYCLE | TIME )
```

This specifies the abscissa type when loading CSV data.

```
input-data ( CA | TIME | RTP_RESULTS | RESULTS_RAW | RESULTS | ALL )
```

Specifies the type of data to load from an AVL IFile.

```
number-of-channels <n>
```

This specifies the number of channels when loading CSV data. If data has already been loaded it will be deleted.

```
number-of-cycles <n>
```

This specifies the number of cycles to load when loading CSV data.

If CSV or IFile data has already been loaded then this will modify the number of cycles as specified.

```
resolution <n>
```

This specifies the resolution of data when loading CSV data. It is either in samples per degree for crank angle data or Hertz for time-based data depending on the setting of input-abcissa-type.

```
recording-length <n>
```

This specifies the recording length in seconds for CSV time-based data as specified with input-abcissa-type.

```
header-lines <n>
```

This specifies the number of lines to ignore at the beginning of a file when loading CSV data.

```
skip-columns <a> <b> <c> ...
```

This specifies the column numbers to skip when importing CSV data. Column numbering starts from one, not zero.

```
reset-columns
```

This resets the columns to be skipped

```
channel-names-line <n>
```

This sets which line of the CSV file the channel names occur.

```
channel-units-line <n>
```

This sets which line of the CSV file the channel units occur.

```
load-channels ( <channel-name1> <channel-name2> ... | #<n1> #<n2> ... | none  
| all )
```

This loads the channels specified, either none, all or the channel names or #numbers specified. The file must have been pre-loaded by specifying the input-file command.

```
channel ( <channel-name> | #<n> | all ) name <name>  
channel ( <channel-name> | #<n> | all ) description <description>  
channel ( <channel-name> | #<n> | all ) units <units>  
channel ( <channel-name> | #<n> | all ) slope <slope>  
channel ( <channel-name> | #<n> | all ) offset <offset>  
channel ( <channel-name> | #<n> | all ) tdc-offset <tdc-offset>  
channel ( <channel-name> | #<n> | all ) cylinder <n>  
channel ( <channel-name> | #<n> | all ) type <type>  
channel ( <channel-name> | #<n> | all ) analysis-info
```

```

channel <channel-name> rename <new-channel-name>
channel <channel-name> info
channel <new-channel-name> create
channel <channel-name> copy <new-channel-name>
channel <channel-name> create-time <new-channel-name> <resolution>
channel <channel-name> convert-to-time <resolution>
channel <channel-name> delete
channel <channel-name> generate sin <frequency>
channel <channel-name> generate block <start> <finish>
channel <channel-name> generate cps <ppr>
channel <channel-name> sample <other-channel> <align-tdc>

```

**Valid channel types:** ENG\_SPEED, CYLPR, INJPR, NEEDLELIFT, VALVELIFT, INLETPR, EXHPR, LOWT, HIGHT, SPKPRICURR, SPKSECCURR, BLOCKACC, IGNANG, CPS, CID, INJECTOR, TIME, FRP, RESULTS, SCALAR, STATEVAR, CAN, DIGITAL, STD\_RESULTS, LS\_DAQ, TEMPERATURE, PRESSURE, OPTRAND\_DIAG, TOOTH\_PERIODS, VIRTUAL, GENERIC, INJECTOR\_CURR, VOLUME.

```

channel ( <channel-name> | all ) soc
    start_window <angle>
    finish_window <angle>
    value <value>
    channel <name>
    aligned (0|1)
    invert (0|1)
    type ( NONE | FIXED | CA_CHANNEL_RISE_RATE | CA_CHANNEL_FALL_RATE |
    CA_CHANNEL_AVERAGE | CYCLE_CHANNEL | DIGITAL_FALLING_EDGE |
    DIGITAL_RISING_EDGE | POSITIVE_HR )

```

```

channel ( <channel-name> | all ) channel-offset
    fixed_value <value>
    start_window <angle>
    finish_window <angle>
    polytropic_index <index>
    calc_interval <interval>
    channel <name>
    truncate <0|1>
    type ( NONE | FIXED | POLYTROPIC | POLYTROPIC_2PT | POLYTROPIC_3PT
    | WINDOW | WINDOW_ABS | MEAN | OTHER )

```

```

channel ( <channel-name> | all ) abscissa
    show
    clear
    resample
    add <start-angle> <finish-angle> <resolution>

```

```

channel ( <channel-name> | all ) filter
    type <type>
    upper_frequency <hz>
    lower_frequency <hz>
    now
    force

```

```

channel ( <channel-name> | all ) digitize
    type

```

```
set-high
clear-low
filter
invert
```

## engine

```
name <name>
evo_ca <n>
evc_ca <n>
ivo_ca <n>
ivc_ca <n>
bore <n>
stroke <n>
conrod_length <n>
pin_offset ( <cylinder-number> | all ) <n>
compression_ratio <n>
cylinders <n>
strokes <2|4>
type ( SI | DISI | CI_DI | CI_IDI | SI_ROTARY )
piston_factor <n>
info
custom-volume <filename>
```

## load-file

Loads a CSV or IFile using as configured by input-file-type and input-file.

## set

```
comment
parameter-file <filename>
date
parameter (0-27) <name> <units> <value>
parameter show
eeoc_start_window
eeoc_finish_window
fft_start_window
fft_finish_window
eeoc_index
t_ivc
temp_ref_ca
mfb_n
annand_a
t_wall
R
poly_exp_start_angle
poly_exp_finish_angle
poly_comp_start_angle
poly_comp_finish_angle
pkp_start_angle
pkp_finish_angle
pkp_smoothing_range
pkp_smoothing_resolution
pressure_rise_start_angle
pressure_rise_finish_angle
pressure_rise_range
cd_start_angle
```

```

cd_finish_angle
engine_speed
injector_start_window
injector_finish_window
max_number_of_injections
align_injections_to_tdc
interpolate_mfb
restrike_analysis
misfire_imep
slowburn_imep
knock_pkp
mega_knock_pkp
knock_kbf
mega_knock_kbf
knock_knkbint
mega_knock_knkbint
tla_range
wiebe_a_start
wiebe_a_finish
wiebe_a_step
wiebe_m_start
wiebe_m_finish
wiebe_m_step
engine_speed_channel
knock_integral_type ( RECTIFIED_INTEGRAL | SQUARED_INTEGRAL )
engine_speed_type ( NOTHING | SPECIFY | CHANNEL_AVERAGE | IFILE )
heat_release_mode 1 ( FIRST_LAW | POLY_FIRST | AVL_THERMO1 )
heat_transfer_model ( ANNAND | WOSCHNI | HOHENBERG | EICHELBERG |
NUSSELT | BRILING )

```

output-file <filename> <force-overwrite>

Specifies the filename of the output file. Use 'force-overwrite' to be able to set the input and output filename the same.

```
output-file-type ( IFILE | CSV | MATLAB | ATIMAT )
```

Specified the file type of the output file.

```
output-data ( CA_RAW | CA | CA_TO_TIME | TIME | RTP_RESULTS | RESULTS |
RESULTS_RAW | ALL )
```

Specifies which types of data to output. Use a minus at the beginning of a type to remove, i.e.

```
output-data ALL -TIME
```

```
analyse
  all
  none
  BURN_ANGLE_[1,2,5,10,20,25,50,75,80,90,95,98,99]
  BURN_DURATION_[0_2,0_5,0_10,0_90,2_90,5_90,10_90]
  CENTRE_OF_GRAVITY
  CID_ANGLE
  DWELL_TIME
  EEOC

```

END\_OF\_INJECTION\_[1,2,3,4,5,6]  
ENGINE\_SPEED  
EXHAUST\_VALVE\_CLOSING  
EXHAUST\_VALVE\_OPENING  
GROSS\_IMEP  
INDICATED\_POWER  
INDICATED\_TORQUE  
INDICATED\_TORQUE\_LBFT  
INDICATED\_TORQUE\_NET  
INJECTOR\_DURATION\_[1,2,3,4,5]  
INJECTOR\_SEPARATION\_[1,2,3,4,5]  
INLET\_VALVE\_CLOSING  
INLET\_VALVE\_OPENING  
KNOCK\_BOSS\_FACTOR  
KNOCK\_BOSS\_INTEGRAL  
KNOCK\_FACTOR  
KNOCK\_INTEGRAL  
KNOCK\_C\_AND\_D  
KNOCK\_C\_AND\_D\_CA  
KNOCK\_ONSET\_CA  
KNOCK\_ONSET\_UMFB  
LOWER\_PUMPING\_IMEP  
MAXIMUM\_VALUE  
MAX\_BURN\_RATE  
MAX\_BURN\_RATE\_CA  
MAX\_COIL\_CURRENT  
MAX\_HEAT\_RELEASE\_RATE  
MAX\_HEAT\_RELEASE\_RATE\_CA  
MAX\_MEAN\_GAS\_TEMP  
MAX\_MEAN\_GAS\_TEMP\_CA  
MAX\_PRESSURE  
MAX\_PRESSURE\_CA  
MAX\_PRESSURE\_IVO  
MAX\_PRESSURE\_IVO\_CA  
MAX\_PRESSURE\_RISE\_RATE  
MAX\_PRESSURE\_RISE\_RATE\_CA  
MEAN\_VALUE  
MINIMUM\_VALUE  
MIN\_PRESSURE  
MIN\_PRESSURE\_CA  
MIN\_PRESSURE\_EVC  
MIN\_PRESSURE\_EVC\_CA  
MISSING\_TOOTH\_1  
MISSING\_TOOTH\_2  
MISSING\_TOOTH\_RATIO\_MAX  
MISSING\_TOOTH\_RATIO\_MIN  
NET\_IMEP  
NUMBER\_OF\_INJECTIONS  
PRESSURE\_OFFSET  
PEAK\_KNOCKING\_PRESSURE  
PEAK\_KNOCKING\_PRESSURE\_CA  
POLY\_COMP  
POLY\_EXP  
PUMPING\_IMEP  
RESTRIKE\_DELAY\_TIME  
RESTRIKE\_DWELL\_TIME

RESTRIKE\_MAX\_CURRENT  
 RESTRIKE\_TIMING  
 START\_OF\_COMBUSTION  
 START\_OF\_INJECTION\_[1,2,3,4,5,6]  
 TLA  
 TOOTH\_GAP\_RATIO\_MAX  
 TOOTH\_GAP\_RATIO\_MIN  
 TOTAL\_HEAT\_RELEASE  
 UPPER\_PUMPING\_IMEP  
 WIEBE\_A  
 WIEBE\_M  
 FFT  
 FFT\_REFERENCE  
 FFT\_TORQUE\_SUM  
 FFT\_KNOCK\_PRESSURE  
 ANGULAR\_TORQUE  
 ANGULAR\_TORQUE\_SUM  
 DIGITAL\_SIGNAL  
 GAMMA  
 GROSS\_HEAT\_RELEASE\_RATE  
 H\_COEFF  
 KNOCKING\_PRESSURE  
 MEAN\_GAS\_TEMP  
 MFB  
 MOTORED\_PRESSURE  
 MOVING\_PRESSURE\_AVERAGE  
 NET\_HEAT\_RELEASE\_RATE  
 POLYFIT  
 POLYTROPIC\_INDICES  
 PRESSURE\_RISE\_RATE  
 TOOTH\_SPEED  
 WIEBE\_MFB

Multiple items can be specified on one line. Use of a minus sign before the analysis type negates that analysis.

Example:

```
analyse all -WIEBE_A -WIEBE_M
```

Would run configure catool to run all analysis except Wiebe a and m parameter calculations. Because the analysis does not run until the run-analysis command you can specify numerous lines to build up the necessary analysis configuration.

run-offset-correction

Allows offset correction to be performed without any other analysis

run-analysis

Runs the analysis configured using analyse.

configure-analysis

Configures analysis such that `channel <channel-name> analysis-info` lists the analysis channels that will be calculated.

`output`

This outputs to the file specified by `output-file` the data specified with `output-data` in the file type specified by `output-file-type`.

`print <message>`

This displays the text specified so long as the debugging level is not set to FATAL or SILENT.

`stop`

Immediately stops the parsing of the config file.

`threads <n>`

Specifies the number of threads that catool should use. This should be set to the total number of processor cores the machine has.



# Calculations

## Heat Release

Burn rate analysis is commonly used with spark ignition engines to determine the mass fraction burned. Rassweiler and Withrow<sup>13</sup> developed a technique in 1938 that is still considered today to be both accurate and computationally efficient.

During combustion, the pressure rise,  $\Delta p$ , during a crank interval,  $\Delta \theta$ , is considered to consist of pressure rise due to combustion,  $\Delta p_c$ , and pressure change due to change in volume,  $\Delta p_v$ .

$$\Delta p = \Delta p_c + \Delta p_v$$

As the crank angle increments from  $\theta_i$  to  $\theta_{i+1}$  the volume changes from  $V_i$  to  $V_{i+1}$  and the pressure from  $p_i$  to  $p_{i+1}$ . Assuming that the change in pressure due to volume change can be calculated from a polytropic process of constant  $k$ :

$$p_{i+1} - p_i = \Delta p_c + p_i \left[ \left( \frac{V_i}{V_{i+1}} \right)^k - 1 \right]$$

hence

$$\Delta p_c = p_{i+1} - p_i \left( \frac{V_i}{V_{i+1}} \right)^k$$

Because the combustion process does not occur at constant volume, the pressure rise rate due to combustion is not directly proportional to the mass of fuel burned. Therefore the pressure rise due to combustion must be referenced to a datum volume, such as that at TDC,  $V_{tdc}$ .

$$\Delta p_c^* = \Delta p_c \frac{V_i}{V_{tdc}}$$

By identifying the end of combustion and the number of crank angle intervals between start and finish of combustion,  $N$ , the mass fraction burned can be calculated:

$$mfb = \frac{\sum_0^i \Delta p_c^*}{\sum_0^N \Delta p_c^*}$$

## Cycle Based Calculations:

B0002	Angle between SOC (Start of Combustion) and 2% MFB
B0010	Angle between SOC and 10% MFB
B0090	Angle between SOC and 90% MFB

B0590	Angle between 5% and 90% MFB
B1090	Angle between 10% and 90% MFB
MFB01	1% MFB
MFB02	2% MFB
MFB05	5% MFB
MFB10	10% MFB
MFB20	20% MFB
MFB25	25% MFB
MFB50	50% MFB
MFB75	75% MFB
MFB80	80% MFB
MFB95	95% MFB
MFB98	98% MFB
MFB99	99% MFB
MXBRN	Maximum Burn Rate (J/deg)
AMXBRN	Angle of Maximum Burn Rate (deg)

### **Crank Angle Calculations:**

MFB            Mass Fraction Burned (%)

### **CID**

Crank angle of the camshaft ID position

### **EEOC**

The estimated end of combustion (EEOC) is required for determining the normalising value for mass fraction burned and for heat release analysis. There have been several methods suggested by researchers, but the most common is to determine the crank angle that provides a maximum value of equation 4.11.

$$x = p.V^{1.15}$$

In order to reduce the effects of signal noise, the method is modified slightly to determine the crank angle that provides a maximum over a five-point summation of equation 4.11:

$$x = \sum_{i=\theta-2}^{i=\theta+2} p_i.V_i^{1.15}$$

In order to ensure the end of combustion is not underestimated, ten degrees is added to the crank angle at which  $x$  reaches a maximum.

### **Start and End of Injection**

Calculated from injector signal.

## Cycle based calculations:

EOI1_	1 <sup>st</sup> End of Injection (deg)
EOI2_	2 <sup>nd</sup> End of Injection (deg)
EOI3_	3 <sup>rd</sup> End of Injection (deg)
EOI4_	4 <sup>th</sup> End of Injection (deg)
EOI5_	5 <sup>th</sup> End of Injection (deg)
EOI6_	6 <sup>th</sup> End of Injection (deg)
SOI1_	1 <sup>st</sup> Start of Injection (deg)
SOI2_	2 <sup>nd</sup> Start of Injection (deg)
SOI3_	3 <sup>rd</sup> Start of Injection (deg)
SOI4_	4 <sup>th</sup> Start of Injection (deg)
SOI5_	5 <sup>th</sup> Start of Injection (deg)
SOI6_	6 <sup>th</sup> Start of Injection (deg)

N

Engine Speed calculated over one engine cycle. Either two revolutions for a four stroke engine or one revolution for a two strong engine.

## Mean Gas Temperature

The mean gas temperature is required for the calculation of heat release.

for a polytropic process<sup>28</sup>

$$pV^n = \text{constant}$$

$$\left(\frac{T_2}{T_1}\right) = \left(\frac{V_1}{V_2}\right)^{n-1} = \left(\frac{p_2}{p_1}\right)^{\frac{n-1}{n}}$$

hence

$$T_2 = T_1 \left(\frac{V_1}{V_2}\right)^{n-1} = T_1 \left(\frac{p_2}{p_1}\right)^{\frac{n-1}{n}}$$

for a known reference location, such as inlet valve closure:

$$p_{ref} \cdot V_{ref} = n \cdot R \cdot T_{ref}$$

rearranging gives:

$$\frac{T_{ref}}{p_{ref} \cdot V_{ref}} = \frac{1}{n \cdot R}$$

to calculate the temperature at an arbitrary position between inlet valve closure and exhaust valve opening:

$$T_{calc} = p_{calc} \cdot V_{calc} \cdot \frac{1}{n \cdot R}$$

assuming  $n$  and  $R$  remain constant, equation 4.35 can be substituted into equation 4.36:

$$T_{calc} = p_{calc} \cdot V_{calc} \frac{T_{ref}}{p_{ref} \cdot V_{ref}}$$

Cycle calculations:

MXT            Maximum Mean Gas Temperature (K)  
AMXT         Angle of Maximum Mean Gas Temperature (deg)

Crank Angle calculations:

MGTEMP      Mean Gas Temperature (K)

**EVC, EVO, IVC, IVO**

Exhaust Valve Closing, Exhaust Valve Opening, Intake Valve Closing, Intake Valve Opening

**IMEP**

The combustion analysis software calculates indicated mean effective pressure using the following equation:

$$imep = \frac{\Delta\theta}{V_s} \sum p \cdot \frac{dV}{d\theta}$$

This equation has been shown to be both computationally efficient and provide good robustness to coarse crank angle resolutions<sup>14</sup>.

Using the formula between -180 and +180 degrees provides the gross imep and, outside of this range, the pumping imep. The addition of these two parameters provides the net imep that includes the input of energy from combustion and the losses due to pumping.

Additionally, the pumping imep is split at atmospheric pressure between the upper and lower pumping loop imep. The upper pumping loop indicates the amount of energy required to propel the combustion products through the exhaust valve and piping system. The lower loop indicates the losses due to induction, including the throttling losses across the intake valve<sup>33</sup>.

**Cycle calculations:**

GMEP            Gross IMEP (-180 to 180 degrees)  
NMEP            GMEP - PMEP  
UPMEP          Upper pumping IMEP (-360 to -180 and 180 to 360 degrees)  
LPMEP          Lower pumping IMEP (-360 to -180 and 180 to 360 degrees)  
PMEP            UPMEP + LPMEP

**QRTMAX, AQRMTX**

Heat release analysis is generally applied to compression ignition engines, although there is no reason why it cannot be used in spark ignition applications. Heat release analysis computes how

much heat would need to have been added to the cylinder contents, in order to produce the observed pressure variations<sup>8</sup>.

Using the first law of thermodynamics it can be shown<sup>6,8,21</sup>:

$$\frac{dQ_{net}}{d\theta} = \frac{\gamma}{\gamma-1} P \frac{dV}{d\theta} + \frac{1}{\gamma-1} V \frac{dp}{d\theta}$$

where

$\gamma$  is the ratio of specific heats

$Q_{net}$  is the net heat release rate in Joules per degree

$P$  is the in-cylinder pressure in Pascals

$V$  is the in-cylinder volume in cubic metres

By taking into account the effects of heat transfer to the cylinder walls, the gross heat release can be calculated:

$$\frac{dQ_{gross}}{d\theta} = \frac{dQ_{net}}{d\theta} + \frac{dQ_{ht}}{d\theta}$$

$$\frac{dQ_{ht}}{d\theta} = h(T - T_{wall}) \frac{dA}{d\theta}$$

where

$h$  is the heat transfer coefficient

$T$  is the mean gas temperature in Kelvin, calculated from the equation of state ( $pV=mRT$ )

$T_{wall}$  is the mean cylinder wall temperature in Kelvin

$A$  is the instantaneous heat transfer surface area of the combustion chamber in cubic metres

### ***Heat Transfer Coefficients***

Over the years various papers have been published aiming to quantify the heat transfer coefficient to easily measured or derived engine parameters. Some of the most common functions used are implemented in the combustion analysis software and are presented below.

Hohenberg<sup>23</sup>

$$h = 129.8V^{-0.06} p^{0.8} T^{-0.4} (\bar{v}_p + 1.4)^{0.8}$$

Woschni<sup>24</sup>

$$h = 129.8B^{-0.2} p^{0.8} T^{-0.53} \left( C_1 \bar{v}_p + C_2 \frac{V_s T_{ref}}{P_{ref} V_{ref}} (p - P_{motored}) \right)^{0.8}$$

where

$C_1 = 6.18$  in scavenging period

$C_1 = 2.28$  in compression, combustion and expansion

$C_2 = 0$  in scavenging period and compression

$C_2 = 3.24 \times 10^{-3}$  in combustion and expansion

$C_2 = 6.22 \times 10^{-3}$  in combustion and expansion (IDI engines)<sup>8</sup>

Annand<sup>25</sup>

$$h = \frac{a \cdot \lambda}{B} \text{Re}^{0.7} + c \frac{(T^4 - T_{wall}^4)}{T - T_{wall}}$$

where

$$0.35 < a < 0.8$$

$c = 0$  during intake and compression

$c = 0.576 \textcircled{\circ}$  for CI engine combustion and expansion

$c = 0.075 \textcircled{\circ}$  for SI engine combustion and expansion

from Bosch<sup>27</sup>  $\textcircled{\circ} = 5.67 \times 10^{-8} \text{ W} \cdot \text{m}^{-2} \cdot \text{K}^{-4}$

from Street et al<sup>26</sup>

$$\text{Re} = \frac{V \cdot d \cdot \rho}{\mu}$$

where

$V$  is the mean velocity in the pipe (mean piston speed) in metres per second

$d$  the characteristic length (engine bore) in metres

$\rho$  is the density of the fluid in kilograms per cubic metres

$\mu$  is the dynamic fluid viscosity in kilograms per metre per second

Mean piston speed is calculated from engine speed. The software provides two sources of engine speed. The user can either specify it directly or if the engine speed channel has been recorded then the channel number can be specified and the speed averaged over the individual engine cycle periods. Recording engine speed has the benefit of accounting for the continually changing engine speed due to cycle-to-cycle variation of combustion.

$$V = 2 \cdot L \cdot N$$

where

$N$  is engine speed in revolutions per second

$L$  is engine stroke in metres

$$\rho = \frac{P}{R \cdot T}$$

Annand<sup>25</sup> approximates:

$$\lambda = \frac{C_p \cdot \mu}{0.7}$$

from Brunt<sup>6</sup>:

$$C_p = \frac{R}{1 - \frac{1}{\gamma}}$$

$$\gamma = 1.338 - 6.0 \times 10^{-5} T + 1.0 \times 10^{-8} T^2 \quad (\text{based on gasoline engine})$$

The following figures are published:

Brunt:

a=0.45  
R=288.8

Annand:

$\mu = 4.702 \times 10^{-7} T^{0.645}$   
R=241.1